#### **ENGINEERING ANALYSIS**

#### **PROJECT DESCRIPTION**

On December 20, 2024, Hikae Aluminum Processing, L.L.C. (Hikae) submitted an air permit application for the purchase and operation of the Grooms Aluminum Processing (Grooms) facility in Ashville, Alabama. Grooms was a secondary aluminum processing facility that operated a 25-ton rotary melting furnace and associated aluminum shredder, crushers and screeners. Grooms operated under Synthetic Minor Operating Permits (SMOPs) 410-0041-X002 & X003, issued on July 13, 2022. On June 26, 2024, Grooms notified the Department they had stopped all production operations at the facility as of May 30, 2024. Following an inspection of the Grooms facility, by the Department, on June 28, 2024, the Department changed the facility status to ceased and voided the existing SMOPs 410-0041-X002 & X003, on July 3, 2024.

Hikae plans to reopen the Grooms facility and restart the existing equipment. Operations will include scrap aluminum storage, shredding, crushing, screening, melting and casting. The 25-ton rotary furnace, which is heated by a 20.00 MMBtu/hr natural gas burner, will melt, with flux, aluminum scrap and recovered aluminum fines from dross after the crushing and shredding process. The estimated 6.25 ton per hour of molten aluminum would then be poured into molds to solidify and cool prior to storage and sale. Hikae reported they have no plans to install any additional equipment.

Depending on processing need, scrap feedstock will be conveyed through an electric Saturn Shear Shredder (M-240) or directly charged to the furnace after the crushing and screening process. The crushing and screening process consists of a Diamond jaw crusher, a Stedman (M-4230) impact crusher and a Hewitt Robins (VT1503) triple-decker screen, which will be used to both, reduce the size on incoming scrap, and recover aluminum from the furnace dross or salt cake. Aluminum scrap and dross/salt cake will enter the jaw crusher for initial size reduction and then be screened to separate out aluminum fines from dross fines. The recovered aluminum fines would be fed back to the rotary furnace, and dross fines would be discarded. Oversized pieces from the screen would be processed again by the impact crusher and sent back to the screen.

Emissions from the shredding operation will be controlled by wet suppression. Emissions from the crushing and sizing operations are routed to and controlled by a 49,000-cfm Baghouse (BH1); and emissions from the furnace are routed to a spark arrestor and then to a 30,000-cfm lime injected Baghouse (BH2).

#### EMISSIONS

Per ADEM Admin. Code r. 335-3-14-.04, Potential to Emit shall mean the maximum capacity of a stationary source to emit a pollutant under its physical and operational design. Any physical or operational limitation on the capacity of the source to emit a pollutant, including air pollution control equipment and restrictions on hours of operation or on the type or amount of material combusted, stored, or processed, shall be treated as part of its design if the limitation or the effect it would have on emissions is enforceable.

The Potential to Emit (PTE) from the proposed units is calculated using the maximum capacity of the emissions unit under its physical and operational design for 8,760 hrs per year unless the owner or operator is willing to accept a federally enforceable limitation to lower its PTE. In order to maintain the facility's Synthetic Minor Operating Permits (SMOP), Hikae requested to limit the aluminum processed by the melting furnace to 37,110 tons per year.

Per Hikae's application, Hikae has proposed 6.00 lb/hr and 4.28 lb/hr SMOP limits on total PM from the furnace and crushing and screening operations, respectively. Wet suppression on the shredder's emission

should limit particulate matter sufficiently without the need for an explicit lb/hr limit. Hikae did not specifically request a limit on material processed by the crushers and shredders; however, in order to maintain potential emissions below the major source thresholds criteria pollutants, and single HAP pollutants, Hikae estimated the PTE from aluminum scrap processed by the shredder based on maximum capacity of 54,330 TPY (37,110 tpy aluminum scrap and 17,220 tpy waste material) and material processed by the crushers and screener based on a maximum capacity of 40,166 tons per year (37,110 TPY aluminum scrap and 3,035 tpy recycled dross). The additional material charged to the crushers and screener accounts for the reprocessing of the dross and aluminum fines recycled from the furnace. Hikae based PTE on 5433 hours per year as needed, except for furnace heater emissions which were based on operating at 8760 hours per year. Where needed, calculations are based on 6.83 TPH (37,110 TPY) scrap and 0.56 TPH solid flux charged to the rotary furnace and a 6.5 TPH (33,956 TPY) molten aluminum and 1.14 TPH salt cake output from the furnace.

	Summary of Emission Units and Throughputs								
		Rate	d Capacit	ty	Maximum				
Emission	Description	Natural	Δίμη	ninum	Operating				
Unit	Description	Gas	Лип	iniuni	Hours				
		MMBtu/hr	TPH	TPY	HPY				
FSS	Shear Shredder	-	10.0	54,330	5,433				
AC	Crushing and Screening	-	7.39	40,166	5,433				
RF	Furnace Heater	20.0	-	-	8,760				
RF	Furnace Melt/Charge	-	6.83	37,110	5,433				
RF	Furnace melt/Production	-	6.50	33,956	5,433				

The maximum rated capacities and potential annual throughputs for the emissions units associated with this project are shown below in Table 1.

Table 1

Emissions from the shredder are controlled by wet suppression. Hikae estimated the emission reduction due to wet suppression at 50%. The use of wet suppression by Hikae would be required on an as needed bases, based on visible emission observations during operation. Emissions from the crushing and screening process are directed to and controlled by a fabric filter baghouse (BH-1). The Department assumes 90% collection efficiency to BH-1, and based on Hikae's application, specific pollutant minimum control efficiencies of PM at 83.5%, PM<sub>10</sub> at 80.2%, PM<sub>2.5</sub> at 67%, and MHAPs at 83.6%. These control efficiencies were used to provide conservative estimates. Actual control efficiencies are expected to be higher. Emissions from the rotary melting furnace are routed to and controlled by a lime injected baghouse (BH-2). The Department assumes 90% collection efficiencies of PM at 89%, PM<sub>10</sub> at 89%, PM<sub>10</sub> at 87%, and PM<sub>2.5</sub> at 79%. Based on previous testing at the facility, HCI emissions were assumed to be at the requested emission limit of 3.5 lb/hr (9.5 TPY). Since the use of wet suppression of shredder emissions and the use of (BH-1) are not required as part of their design, the PTE does not account for controlled emissions from these sources. For calculation purposes, operating hours were normalized to 5937 hrs/yr based on the proposed 37,110 TPY production limit.

Emission control of group 1 furnaces is required by 40 CFR Part 63 Subpart RRR. The inclusion of BH-2's capture and control efficiency were included in the PTE estimates for the furnace only. The use of this

control device is enforceable and is therefore considered part of the operational design of the furnace emission source at the facility.

Dioxin and furan (D/F) PTE is based on the limit stipulated by 40 CFR Part 63 Subpart RRR (2.10 gr-DF/ton-charge). Estimates of uncontrolled HAP emissions of 3.87 lbs of HCL per ton of charge to the furnace are factors derived from similar tests at similar facilities.

The emission factors utilized for calculation of PTE were developed or adapted from the following sources:

- Condensable Particulate Matter (PMcon) included with PM<sub>10</sub>, and PM<sub>2.5</sub> emission factors in accordance with USA EPA's October 2012 final NSR rule (77 FR 65107) (40 CFR parts 51 and 52).
- Natural Gas Combustion-emission factors (other than PM) were derived from US EPS AP-42 Chapter 1.4.
- Natural Gas Combustion PM<sub>T</sub>, PM<sub>2.5</sub>, PM<sub>10</sub> (filterable plus condensable) emission factors were derived from US EPA 2002 National Emission Inventory (NEI) Data and supporting documentation.
- Metal and Organic HAP emissions from furnace melting were derived from "Development of the RTR Supplemental Proposal Risk Modeling Dataset for the Secondary Aluminum Production Source Category, RTI International, 12/7/14".
- Furnace PM emissions were derived from EPA Emission Factor Listing for Criteria Pollutants, EPA 450/4-90-003, and AP-42, Chapter 12.8 "Secondary Aluminum Operations".
- Emissions from furnace material handling and hot dross handling were derived from AP-42, Chapter 12.5.1 "Steel Minimills".
- PM emissions from stored and stockpiled material were derived from AP-42, Chapter 13.2.5 "Industrial Wind Erosion".
- Furnace emissions of NO<sub>x</sub>, PM<sub>con</sub>, and CO were derived from a 90% UPL analysis of isolated sidewell stack test results from reverb type furnaces.
- Furnace HCL emissions were based on conservative emission estimates from a similar facility provided by Hiake "Schnitzer Steel Industries, Inc., "Supplemental Information for NOC 11986-General Metals of Tacoma, Washington, date June 28, 2023".
- Historical and recent emissions testing data and vendor provided emission data.
- GHG emissions were obtained from 40 CFR Part 98, Subpart C, Tables C-1 and C-2.

Pollutant (TPY)	Heater	Furnace Fug + Controlled	Fugitives <sup>1</sup>	Total Emissions
<b>PM</b> <sub>Total</sub>	0.65	4.87	45.60	51.12
PM <sub>filt</sub>	0.16	4.08	45.60	49.84
PM <sub>10,filt</sub>	0.16	3.37	4.92	8.45
PM <sub>2.5,filt</sub>	0.16	3.89	4.82	8.88
PMcon	0.49	0.80	-	1.29
SO <sub>2</sub>	0.05	0.05	-	0.10
NO <sub>X</sub>	8.59	1.49	-	10.07
со	7.21	13.52	-	20.74
VOC	0.47	42.45	3.83	46.75
Total HAPs	0.16	10.67	1.02	11.85
M-HAPs	-	1.89E-03	0.23	0.23

#### Table 2: Potential Emissions

O-HAPS	-	1.14	0.79	1.93
HCL	-	9.53	-	9.53
D/F	-	5.57E-07	-	5.57E-07
CO <sub>2</sub>	10247.10	-	-	10247.10
N <sub>2</sub> O	0.02	-	-	0.02
CH₄	0.19	-	-	0.19
Mass Sum	10247.32	-	-	10247.32
CO <sub>2e</sub>	10257.69	_	-	10257.69

<sup>1</sup> Includes emissions from shred/crush/screen, material handling, pouring and cooling.

#### LIMITS

In addition to the D/F limit required by 40 CFR Part 63 Subpart RRR (2.10 gr-DF/ton-charge), Hikae has requested SMOP limits of 37,110 TPY for aluminum scrap melting; 54,330 TPY from shredding; 40,116 TPY for crushing and screening; 6.0 lb/hr PM and 3.50 lb/hr HCl from the melting furnace; and 4.28 lb/hr of PM from crushing and screening operations. In addition, process operating hours will be limited to 5,433 hours per year.

#### REGULATIONS

#### ADEM Administrative Code Rule 335-3-4-.01(1)(a and b), "Visible Emission"

**ADEM 335-3-4-.01(a)** states that no person shall emit to the atmosphere particulate of an opacity of greater than twenty percent (20%) over a six (6) minute period. **ADEM 335-3-4-.01(b)** states that during one sixminute period in any sixty-minute period a person may discharge into the atmosphere from any source of emissions, particulate of an opacity not greater than that designated as forty percent (40%) opacity. All sources, including both baghouses, the meltshop roof vents, and any other openings in the building or sources located outside are subject to this rule.

For Hikae to maintain compliance with these rules, Hikae shall perform daily visible emission checks of each unit when operating. If visible emissions are noted, Hikae shall perform a visible emissions observation in accordance with Method 9 and take appropriate actions necessary to eliminate the observed emissions immediately, followed by an additional observation to confirm that emissions are reduced to normal. Records of emissions observations, Method 9 observations conducted, including results and any repairs or observed problems, should be noted in a form suitable for inspection.

#### ADEM Administrative Code Rule 335-3-4-.04, "Process Industries - General"

According to **ADEM 335-3-4-.04(1)**, Class 1 Counties: No person shall cause or permit the emission of particulate matter in any one hour from any source in a Class 1 County in excess of the amount determined by the following equations:

$$E = 3.59P^{0.62} \quad E = 17.31P^{0.16}$$
$$(P < 30\frac{tons}{hr}) \quad (P > 60\frac{tons}{hr})$$

Where *E* = emissions in pounds per hour  $\left(\frac{lbs}{hr}\right)$  and *P* = process weight per hour in tons per hour  $\left(\frac{tons}{hr}\right)$ . The shredder, crushers and screen, and furnace at the Hikae facility would be subject to this regulation. These

units are expected to comply with the emission limits based on the throughput limits in Table 1 and potential emissions in Table 2 above. Throughput records shall be kept daily in order to show compliance with the process weight rule.

# ADEM Administrative Code Rule 335-3-14-.04, "Prevention of Significant Deterioration (PSD) Permitting"

Secondary Metal Production facilities are one of the 28 source categories listed in ADEM Admin Code r. 335-3-14-.04(2)(a)1 as having a 100 TPY major source threshold for criteria pollutants. Based on the emissions found in Table 2, the facility would not be expected to exceed the 100 TPY threshold. A facility must address PSD regulations for greenhouse gases only if that facility is major for criteria pollutants. Per ADEM Code r. 335-3-14(2)(a)1(i)&(ii), no PSD review would be necessary for this facility.

## ADEM Administrative Code, Rule 335-3-14-.06, "Determinations for Major Sources in Accordance with Clean Air Act Section 112(g)"

This regulation applies to major sources of hazardous air pollutants (HAPs) constructed after March 27, 1998. Since this facility is not a major source of HAPs, a 112(g) case by case MACT review would not be necessary.

# ADEM Administrative Code, Rule 335-3-15, "Synthetic Minor Source Operating Permits (SMOPs)" and 335-3-16, "Major Source Operating Permits (MSOPs)"

After considering the TPY limits on the sources at the Hikae facility and the overall PTE considering pollution controls, the facility does not have the potential to emit greater than 100 TPY of any single criteria pollutant. The 3.5 lb/hr limit on HCI emissions from the furnace would restrict the facility to less than 10 TPY of any single HAP, after which the facility would not be expected to emit more than 25 TPY of all HAPs species. Given the above limits, the facility will be considered a synthetic minor source for both criteria pollutants and HAPs.

In order to ensure compliance and to match the testing required by 40 CFR Part 63 Subpart RRR, Hikae shall conduct an initial performance test to demonstrate compliance with the above SMOP limits within 180 days of beginning operation. Subsequent performance tests shall be conducted every 5 years.

Hikae must install and operate a device that measures and records or otherwise determines the weight of feed/charge (or throughput) for each operating cycle or time period used in the performance test; and operate each weight measurement system or other weight determination procedure in accordance with the OM&M plan.

#### Class I Area

The nearest Class I Area to Hikae, the Sipsey Wilderness Area, is greater than 100 km from the faciality. Emissions from the proposed project are not expected to have a significant impact on this area.

### FEDERAL REGULATIONS

#### 40 CFR 60 "New Source Performance Standards"

No subparts within this part and applicable to the Hikae facility.

#### 40 CFR 63 "General Provisions"

This subpart is applicable provided that the facility is subject to one of the applicable subparts found under 40 CFR Part 63 "National Emission Standards for Hazardous Air Pollutants for Source Categories".

#### 40 CFR 63 Subpart RRR – NESHAP for Secondary Aluminum Production

This regulation is applicable to each secondary aluminum production facility as defined in §63.1503, at both major and area sources. This includes any establishment using clean charge, aluminum scrap, or dross from aluminum production, as the raw material and performing one or more of the following processes: scrap shredding, scrap drying/delacquering/decoating, thermal chip drying, furnace operations (i.e., melting, holding, sweating, refining, fluxing, or alloying), recovery of aluminum from dross, in-line fluxing, or dross cooling.

Shredded scrap aluminum will be melted and refined within the rotary melting furnace, which is a Group-1 furnace as defined in §63.1503. Therefore, the furnace would be subject to the PM, HCL, HF and Dioxins/Furans (D/F) emission standards found in Subpart RRR §63.1505(i) & (j). However, due to the SMOP limits on HCL and the TPY of charge limit to the furnace, the facility will be considered an area source under this subpart. Therefore, the furnace will only be subject to the D/F emission standards and associated operating, monitoring, reporting and recordkeeping requirements [§63.1500(c)(4)]. Shredders are subject to this subpart, but only at major sources of HAPs.

#### <u>Limits</u>

**Melting Furnace:** Hikae must comply with the 2.1 x 10<sup>-4</sup>gr of D/F TEQ per ton of feed/charge emission standards found in Subpart RRR §63.1505(i)(3).

#### **Operating Requirements**

Hikae must operate all affected sources and control equipment according to the requirements in §63.1506 and, at all times, must operate and maintain any affected source, including associated air pollution control equipment and monitoring equipment, in a manner consistent with safety and good air pollution control practices for minimizing emissions [§63.1506(a)(5)].

#### Labeling

Hikae must provide and maintain easily visible labels posted at the furnace that identifies the applicable emission limits and means of compliance, including: (1) The type of affected source or emission unit (e.g., group 1 furnace). (2) The applicable operational standard(s) and control method(s) (work practice or control device). This includes, but is not limited to, the type of charge to be used for a furnace (e.g., clean scrap only, all scrap, etc.), flux materials and addition practices, and the applicable operating parameter ranges and requirements as incorporated in the OM&M plan [§63.1506(b)].

#### Capture/collection systems

For each affected source or emission unit equipped with an add-on air pollution control device, Hikae must: (1) Design and install a system for the capture and collection of emissions to meet the engineering standards for minimum exhaust rates or facial inlet velocities as contained in the ACGIH Guidelines (incorporated by reference, see § 63.14); (2) Vent captured emissions through a closed system, except that dilution air may be added to emission streams for the purpose of controlling temperature at the inlet to a fabric filter; and (3) Operate each capture/collection system according to the procedures and requirements in the OM&M plan [§63.1506(c)].

#### Feed/charge weight

Hikae must: (1) install and operate a device that measures and records or otherwise determine the weight of feed/charge (or throughput) for each operating cycle or time period used in the performance test; and (2) operate each weight measurement system or other weight determination procedure in accordance with the OM&M plan. Hikae may choose to measure and record aluminum production weight from an affected source or emission unit rather than feed/charge weight to an affected source or emission unit, provided that, all calculations to demonstrate compliance with the emission limits for are based on aluminum production weight rather than feed/charge weight [§63.1506(d)].

#### **Rotary Melt Furnace and Lime Injected Baghouse**

Hikae must operate this unit according to the requirements in 63.1506(m). Hikae has elected to install a bag leak detection system, which must be operated according to 63.1506(m)(1), including: Initiating corrective action within 1 hour of a bag leak detection alarm according to the corrective action procedures in the OM&M plan and operate each fabric filter system such that the bag leak detection system alarm does not sound more than 5 percent of the operating time during a 6-month block reporting period, which is calculated according to 63.1506(m)(1)(iii).

The 3-hour bock average temperature at the inlet of the baghouse shall be maintained less than 25 °F above the temperature established in the most recent performance test and the lime feed hopper shall be free-flowing at all times with the feeder set at or above the level established in the most recent performance test [§63.1506(m)(3)&(4)].

Hikae must maintain the total reactive chlorine flux injection rate for each operating cycle or time period used in the performance test at or below the average rate established during the performance test [§63.1506(m)(5)].

The operation of capture/collection systems and control devices associated with natural gas-fired, group 1 furnaces that will be idled for at least 24 hours after the furnace cycle has been completed may be temporarily stopped. Operations of these capture/collection systems and control devices must be restarted before feed/charge, flux or alloying materials are added to the furnace [§63.1506(m)(7)]. Corrective actions shall be initiated as needed per §63.1506(p).

#### **Monitoring Requirements**

Hikae must monitor all control equipment and processes according to the requirements of §63.1510 including the following: Hikae must prepare and implement an OM&M plan [§63.1510(b)&(s)], maintain and inspect Subpart RRR identification & compliance labels [§63.1510(c)], maintain and inspect the hoods and ductwork including conducting annual flow measurements [§63.1510(d)], maintain and operate scales or other devices to record the total weight of feed/charge to each unit [§63.1510(e)] calculate and record the total reactive flux injection rate (TRFIR) for each operating cycle or time period used in the performance test using the procedure in § 63.1512(o) [§63.1510(j)(2)]. Record, for each 15-minute block period during each operating cycle or time period used in the performance test during which reactive fluxing occurs, the time, weight, and type of flux for each amount of gaseous or liquid flux other than chlorine and solid reactive flux [§63.1510(j)(3)]. For solid flux that is added intermittently, record the amount added for each operating cycle or time period used in the performance test using the procedure in the performance test using the procedure in the performance of gaseous or liquid flux other than chlorine and solid reactive flux [§63.1510(j)(3)]. For solid flux that is added intermittently, record the amount added for each operating cycle or time period used in the performance test using the procedures in § 63.1510(j)(4)].

For the furnace baghouse, Hikae must maintain and continuously operate the bag leak detection system according to the requirements of (1,1)(i)(i)(x); maintain and operate a thermocouple at the inlet of the baghouse [(3,1510(h)(1))] that meets the performance and equipment specifications of (3,1510(h)(2)(i)-(iii)); and, maintain and operate a continuous lime injection system for the baghouse and verify that the lime is always free flowing according to the requirements of (3,1510(h)(2)(i)-(ii)); and the meet a continuous lime injection system for the baghouse and verify that the lime is always free flowing according to the requirements of (3,1510(i)(1)-(4)).

#### Performance Testing

Hikae must conduct performance testing as required by §63.1511 including, submitting a site-specific test plan which satisfies the of all the rule requirements, and must obtain approval of the plan, by the Department, pursuant to the procedures set forth in 40 CFR §63.7. Hikae shall conduct the initial performance test on D/F emissions within 180 days of beginning operation [§63.1511(b)] and subsequent performance tests every 5 years thereafter [§63.1511(e)]. In addition, Hikae must use the required test methods (Method 23 in Part 60 Appendix A) as described in §63.1511(c) or alternatives in §63.1511(d). Operational standards including lime injection rate, baghouse inlet temperature, and total reactive chlorine flux injection rates shall be established [§63.1511(g), §63.1512(d), (k), (n-p)].

#### Notifications, Reports and Record Keeping Requirements

In addition to the recordkeeping required by Subpart A [ $\S63.10(b)$ ], Hikae must maintain records of the operating hours of the furnace, each baghouse leak detection system alarm, plus corrective actions taken [ $\S63.1517(b)(1)(i)$ ], lime injection inspections and feeder settings [ $\S63.15.17(b)(4)$ ], flux additions [ $\S63.1517(b)(5)$ ], charge/feed additions [ $\S63.1517(b)(7)$ ], label inspections [ $\S63.1517(b)(13)$ ], fume hood & ductwork annual inspections [ $\S63.1517(b)(14)$ ], the OM&M plan [ $\S63.1517(b)(16)$ ], and records of deviations and corrective actions taken [ $\S63.1517(b)(14)$ ].

Hikae must submit initial notifications and notifications of compliance status as required by §63.1515(a)&(b) and submit excess emissions/summary reports within 60 days after the end of each 6-month period, as required by §63.1516(b). Malfunctions must be reported per §63.1516(d).

### RECOMMENDATIONS

The facility, as proposed, should be able to meet all state and federal regulations, if operated properly. As such, I recommend Hikae be issued Synthetic Minor Operating Permit Nos. 410-0041-X002 & X003 for the emission units at the Hikae facility pending fee payment.

Draft David DiFante Date **Industrial Minerals Section Energy Branch** Air Division

#### HIKAE ALUMINUM PROCESSING, L.L.C. ASHVILLE, ALABAMA SMOPS: 410-0041-X002 & X003

Data:	Rotary 6.25 T	on Heat	er Emissio	ons		AP-42	EF (NG)	Based on	NG with E	Btu/Conten	t of 1020	
I₂S mol%	0.00%	mol%			PM <sub>filt</sub> =	1.9	Lb/MMScf	(Т	able C-1 & C	;-2)	*Revised 11	/29/2013
Op Hours	8760	Hrs	(normaliz	ed)	PM <sub>con</sub> =	5.7	Lb/MMScf		Part 98 Sub			
leat Content	1,030	Btu/scf (	Ind.)		NO <sub>X</sub> =	100	Lb/MMScf	Emiss	ion Factors	for C <sub>1</sub>		
lowrate	19.417	MScf/Hr	(Ind.)		CO=	84	Lb/MMScf	N <sub>2</sub> 0=	0.0001	kg/MMBtu		
leat Input	20,000,000	Btu/hr			VOC=	5.5	Lb/MMScf	CO <sub>2</sub> =	53.06	kg/MMBtu		
Use btu/scf(EF	PA) for PM, NOx	, CO, VO	C. Factors		HAP=	1.89	Lb/MMScf	CH <sub>4</sub> =	0.001	kg/MMBtu		
or EPA STP (a	Iso ADEM STP)	. SO2 fact	or already		SO <sub>2</sub> =	0.60	Lb/MMScf	(T	able C-1 & C	:-2)		
	STP (from Al.				GW				Part 98 Sub			
nd. STP:	68		14.696		N <sub>2</sub> O=	298			ion Factors	j		
EPA STP:	68		14.696	psia	CO <sub>2</sub> =	1		N <sub>2</sub> 0=		kg/MMBtu		
Heat Content	1,030	Btu/scf (	EPA)		CH <sub>4</sub> =	25		CO <sub>2</sub> =		kg/MMBtu		
uel HHV Corr	ection Factor	1.010						CH <sub>4</sub> =	0.003	kg/MMBtu		
	-		-				on Calculatio	ons				
PMfilt	1.9	Lb	20.000	MMBtu	Scf (	EPA)	8,760 Hr	1 Ton	1.010		0.163	Tons
	MMScf (E	EPA)		Hr	1,030	Btu	Year	2,000 Lb			Ye	ar
PMcon	5.7	Lb	20.000	MMBtu	Scf (	EPA)	8,760 Hr	1 Ton	1.010		0.490	Tons
FINCON	MMScf (E	PA)		Hr	1,030	Btu	Year	2,000 Lb			Ye	ar
	0.60	Lb	20.000	MMBtu	Scf (	EPA)	8,760 Hr	1 Ton	1.010		0.052	Tons
SO <sub>2</sub>	MMScf (E	PA)		Hr	1,030	Btu	Year	2,000 Lb			Ye	ar
NOx	100	Lb	20.000	MMBtu	Scf (	EPA)	8,760 Hr	1 Ton	1.010		8.588	
Nox	MMScf (E	EPA)		Hr	1,030	Btu	Year	2,000 Lb			Ye	ar
со	84	Lb	20.000	MMBtu	Scf (	EPA)	8,760 Hr	1 Ton	1.010		7.214	Tons
00	MMScf (E	PA)		Hr	1,030	Btu	Year	2,000 Lb			Ye	ar
VOC	5.5	Lb	20.000	MMBtu	Scf (	EPA)	8,760 Hr	1 Ton	1.010	_	0.472	Tons
VUC	MMScf (E	PA)		Hr	1,030	Btu	Year	2,000 Lb			Ye	ar
HAP	1.89		20.000		Scf (	EPA)	8,760 Hr	1 Ton	1.010		0.162	
	MMScf (E	EPA)		Hr	1,030	Btu	Year	2,000 Lb			Ye	ar
CO <sub>2</sub>	20	MMBtu	53.06	kg	0.001 M	etric Ton	8,760 Hr	1.102	3 Tons		10,247	Tons
002	Hr		М	MBtu	k	g	Year	1 Met	ric Ton		Ye	ar
N <sub>2</sub> O		MMBtu	0.0001	-	0.001 M		0,100 11		3 Tons	=	0.01931	
	Hr		М	MBtu	k	g	Year	1 Met	ric Ton		Ye	ar
CH₄	20		0.001	-	0.001 M		0,100 11		3 Tons	=	0.19312	
	Hr		М	MBtu	k	g	Year	1 Met	ric Ton		Ye	ar
	10	,247.10	Tons	+	0.019		s +	0.1931		=	10,247	
Mass Sum		Year			Ye	ar		Ye	ear		Ye	ar
		CO <sub>2</sub>			1	I₂O		CH₄				
	10,247.10		X 1		0.019		X 298	0.1931		X 25 _	10,258	
CO <sub>2</sub> e			4.83		Ye	ar						
						N <sub>2</sub> O			CH₄			

<sup>1</sup> AP-42 emission factors taken from Chapter 1.4. Based on natural gas with 1020 btu/scf, and corrected in calculations. From Chapter 1.5, propane emission factors are equivalent on a heat basis to methane factors, except the NO<sub>x</sub> factor is 1.5x higher.

### Furnace Emissions and Fugitives from Melting, Material handling, storage, dross handling, and pouring and cooling.

(material handling) <sup>4</sup>			Fugitives (	storage) <sup>5</sup>							
tpy dross & salt cake	(Hiake Ass	sumption)	113539	TPY metal scr	ар						
B lb pmt/ton low silt	0.021344	TPY pmt	0.25	%moisture							
B lb pm10/ton low silt	0.01043	TPY pm10	1.3	mph wind							
b lb pm2.5/ton low silt	0.003881	TPY pm2.5	0.74	pm30 factor							
			0.007554	lb/ton	0.4288	tpy PM					
			0.0032*PN	130*((mph/5)/	`1.3)/((m	oist/2)^1.4	)				
(hot dross handling) <sup>4</sup>			Fugitives (	Pouring/Cool	ing) <sup>7</sup>						
tpy dross & salt cake			37,110	Tons Scrap Ch	narged						
lb pmt/ton	0.53361	TPY pmt	0.02	lb SO <sub>2</sub> /ton ch	arged	0.04851	TPY SO <sub>2</sub>				
				-	-		_				
· ·		•					^				
lb pm2.5/ton	0.4851	TPY pm2.5	0.14	Ib VOC/ton cl	narged	0.33957	IPY VOC				
	F	F			CONTR				10		
											HCL
											90%
		-	•								95%
					Assume	e Building S	ettling Fa	80.0%	80.0%	80.0%	0.0%
Hb VOC/ton aluminur	<del>n (WebFir</del>	e) <sup>2</sup>	<del>3.71</del>	TPY VOC							
lb VHAP/ton aluminu	um (2014 R	TI, max delaq) <sup>1</sup>	1.14	TPY VHAP	Fug + Bu	uild=fugitiv	ve after bu	ilding con	trol		
	um (RRR l	imit)	5.57E-07	TPY D/F	ТРҮ	Controllec	Fugitive	Fug+Build	Total Emisis	sons	
lb PM/ton product <sup>8</sup>			25.98	TPY PM <sub>filt</sub>	PM <sub>filt</sub>	2.57	2.60	0.52	3.09		
ratio PM10:PM (filt) (	(AP42) <sup>3</sup>		15.59	TPY PM <sub>10,filt</sub>	PM <sub>10, filt</sub>	1.82	3.12	0.62	2.45		
ratio PM2.5:PM (filt)	(AP42) <sup>3</sup>		12.99	TPY PM <sub>2.5, filt</sub>	PM <sub>2.5,filt</sub>	2.45	2.60	0.52	2.97		
MHAP% to PMfilt (20	)14 RTI, ma	x furnace) <sup>1</sup>	0.014	TPY mHAP	mHAP	1.35E-03	2.72E-03	5.45E-04	1.89E-03		
Ib NOX/ton aluminu	m (90% UP	L) <sup>6</sup>	1.46	TPY NOX	HCI	2.96	6.57	6.57	9.53		
b Ib PMcon/ton alumir	num (90% l	JPL) <sup>6</sup>	0.80	TPY Pmcon							
b Ib CO/ton aluminum	(90% UPL)	6	13.52	TPY CO							
b Ib VOC/ton (Hikae as	sumption	)	42.45	TPY VOC							
Ib HCI/ton Similar Fa	cility		65.70	TPY HCI							
Ib HF/ton (Hiake assu	umption)		0.17	TPY HF							
nent of the RTR Sunnle	emental Pr	onosal Risk Mo	delina Data	set for the Sec	ondary A	luminum P	roduction	Source Cat	eaory RTLL	nternational	12/7/14
										international)	
• • •								•	gov/webfire	ъ./)	
		-							BONIMEDILLE	-//	-
napter 13.2.5 "Industri	al Wind Er	osion" (https://	/www.epa.	gov/sites/defa	ault/files	/2020-10/d	ocuments	/13.2.5_in	dustrial_wir	nd_erosion.pd	f)
analysis of isolated sid	dewell sta	ck test results f	rom similar	sidewell/reve	erb type	furnaces					
4/90-0003											
	material handling <sup>4</sup> tpy dross & salt cake lb pmt/ton low silt lb pm10/ton low silt lb pm2.5/ton low silt lb pm2.5/ton low silt lb pm2.5/ton low silt lb pm2.5/ton lb pm10/ton lb pm10/ton lb pm10/ton lb pm2.5/ton lb pm2.5/ton lb pm2.5/ton lb pm2.5/ton lb pm2.5/ton lb pm2.5/ton lb pm2.5/ton lb pm2.5/ton lb pm2.5/ton lb pm2.5/ton aluminur lb VHAP/ton aluminur grains DF/ton aluminur lb PM/ton product <sup>8</sup> ratio PM10:PM (filt) MHAP% to PMfilt (2C lb NOX/ton aluminur lb PMcon/ton aluminur lb PMcon/ton aluminur lb PMcon/ton aluminur lb PMcon/ton aluminur lb PMcon/ton aluminur lb PMcon/ton aluminur lb DOC/ton (Hikae ass lb HC/ton Similar Fa lb HF/ton (Hiake assu nent of the RTR Supple www.regulations.gov/ C/ton-aluminum, We napter 12.8 "Secondar napter 13.2.5 "Industri analysis of isolated sid	material handling) <sup>4</sup> tpy dross & salt cake (Hiake Ass         lb pmt/ton low silt       0.021344         lb pm10/ton low silt       0.01043         lb pm2.5/ton low silt       0.003881         hot dross handling) <sup>4</sup> 0.003881         hot dross k salt cake       0.04851         lb pm10/ton       0.4851         lb pm2.5/ton       0.4851         lb bm2.5/ton       0.4851         lb bm2.5/ton       0.4851         lb bm2.5/ton aluminum (WebFir       10         lb VOC/ton aluminum (2014 R       grains DF/ton aluminum (2014 R         grains DF/ton aluminum (RR I       10 PM/ton Product <sup>8</sup> ratio PM10:PM (filt) (AP42) <sup>3</sup> 3         ratio PM2.5:PM (filt) (AP42) <sup>3</sup> 3         ratio PM2.5:PM (filt) (AP42) <sup>3</sup> 10 NOX/ton aluminum (90% UP         lb NOX/ton aluminum (90% UP       10 PMcon/ton al	material handling) <sup>4</sup> tpy dross & salt cake (Hiake Assumption)         lb pmt/ton low silt       0.021344       TPY pmt         lb pm10/ton low silt       0.01043       TPY pm10         lb pm2.5/ton low silt       0.003881       TPY pm2.5         hot dross handling) <sup>4</sup>	material handling) <sup>4</sup> Fugitives f           tpy dross & salt cake (Hiake Assumption)         113539           lb pmt/ton low silt         0.021344         TPY pmt         0.25           lb pm10/ton low silt         0.01043         TPY pm10         1.3           lb pm2.5/ton low silt         0.003881         TPY pm2.5         0.74           lb pm2.5/ton low silt         0.003881         TPY pm2.5         0.74           hot dross handling) <sup>4</sup> Fugitives (         0.0032*PM           hot dross kaslt cake         37,110         0.002           lb pmt/ton         0.53361         TPY pmt         0.02           lb pm10/ton         0.4851         TPY pm10         0.01           lb pm2.5/ton         0.4851         TPY pm2.5         0.14           6.25 TPH Rotary Furnace Emissions (from scrap)         TPH production normalized to prod limit         5937.6           TPH production normalized to prod limit         5937.6         114         grains DF/ton aluminum (WebFire) <sup>3</sup> 3.741           b VOC/ton aluminum (2014 RTI, max delaq) <sup>1</sup> 1.14         grains DF/ton aluminum (2014 RTI, max delaq) <sup>1</sup> 1.14           grains DF/ton aluminum (RRR limit)         5.57E-07         1b PM/ton product <sup>8</sup> 25.98           ratio PM2.5-PM (filt) (	material handling) <sup>4</sup> Fugitives (storage) <sup>5</sup> tpy dross & salt cake (Hiake Assumption)113539 TPY metal scrlb pm1/ton low silt0.021344 TPY pm10.25 %moisturelb pm2/ton low silt0.01043 TPY pm101.3 mph windlb pm2.5/ton low silt0.003881 TPY pm2.50.74 pm30 factor0.0032*PM30*((mph/5)/0.0032*PM30*((mph/5)/hot dross handling) <sup>4</sup> Fugitives (Pouring/Cooltpy dross & salt cake37,110 Tons Scrap Cflb pm1/ton0.53361 TPY pmt0.02 lb SO <sub>2</sub> /ton chlb pm2/ton0.4851 TPY pm100.01 lb NO_/ton cflb pm2.5/ton0.4851 TPY pm2.50.14 lb VOC/ton cllb pm2.5/ton0.4851 TPY pm2.50.14 lb VOC/ton cllb/ton7000 gr/lb35315 TPY Producedlb/ton7000 gr/lb35315 TPY Producedlb VC/ton aluminum (2014 RTI, max delaq) <sup>1</sup> 1.4 TPY VHAPgrains DF/ton aluminum (2014 RTI, max delaq) <sup>1</sup> 1.4 TPY VHAPlb VOC/ton aluminum (90% UPL) <sup>6</sup> 1.3.52 TPY PM <sub>10, filt</sub> ratio PM10:PM (filt) (2014 RTI, max furnace) <sup>1</sup> 0.014 TPY mHAPlb NOX/ton aluminum (90% UPL) <sup>6</sup> 1.3.52 TPY COlb VOC/ton dluminum (90% UPL) <sup>6</sup> 1.46 TPY NOXlb VOC/ton dluminum (90% UPL	material handling) <sup>4</sup> Fugitives (storage) <sup>5</sup> tpy dross & salt cake (Hiake Assumption)         113539 TPY metal scrap           lb pmt/ton low silt         0.021344 TPY pmt         0.25 %moisture           lb pm10/ton low silt         0.01043 TPY pm10         1.3 mph wind           lb pm2.5/ton low silt         0.003881 TPY pm2.5         0.07554 lb/ton         0.4288           0.0032*PM30*((mph/5)^1.3)/((m	Fugitives (storage) <sup>5</sup> tpy dross & salt cake (Hiake Assumption)         113539 TPY metal scrap           lb pmt/ton low silt         0.021344 TPY pmt         0.25 %moisture           lb pm10/ton low silt         0.001043 TPY pm10         1.3 mph wind           lb pm2.5/ton low silt         0.00381 TPY pm2.5         0.74 pm30 factor           0.007554 lb/ton         0.4288 tpy PM           0.0032*PM30*((mph/5)^1.3)/((moist/2)^1.4)           hot dross handling) <sup>4</sup> Fugitives (Pouring/Cooling) <sup>7</sup> tpy dross & salt cake         37,110 Tons Scrap Charged           lb pm10/ton         0.4851 TPY pm10         0.01 lb NO,/ton charged         0.04255           lb pm2.5/ton         0.4851 TPY pm10         0.14 lb VOC/ton charged         0.33957           6.25 TPH Rotary Furnace Emissions (from scrap)         CONTROL FACTOR         Assume Capture to           TPH production normalized to prod limit         5937.6 hr/yr         Assume DeDEffici           lb VAC/ton aluminum (2014 RTI, max delag) <sup>1</sup> 1.14 TPY VHAP         Fug = uncaptured 4           lb VAC/ton aluminum (RRR limit)         5.57E-07 TPY D/F         TPM into the fug till graits           lb NOX/ton aluminum (RRR limit)         5.57E PY PMint         PMint         2.57           MHAP% to PMfilt (2014 RTI, max furnace) <sup>1</sup> 0.44 TPY	material handling) <sup>4</sup> Fugitives (storage) <sup>5</sup> tpy dross & salt cake (Hiake Assumption)         113539 TPY metal scrap           lb pmt/ton low silt         0.021344 TPY pmt0         0.25 %moisture           lb pm1/ton low silt         0.00381 TPY pm20         1.3 mph wind           lb pm2.5/ton low silt         0.00381 TPY pm2.5         0.74 pm30 factor           0.0032*PM30*((mph/5)^1.3)/((moist/2)^1.4)         0.0032*PM30*((mph/5)^1.3)/((moist/2)^1.4)           hot dross handling) <sup>4</sup> Fugitives (Pouring/Cooling) <sup>2</sup> tpy dross & salt cake         37,110 Tons Scrap Charged         0.04851 TPY SO2           lb pm1/ton         0.53361 TPY pm10         0.01 lb NO,/ton charged         0.04255 TPY NOX           lb pm2.5/ton         0.4851 TPY pm2.5         0.14 lb VOC/ton charged         0.33957 TPY VOC           6.25 TPH Rotary Furnace Emissions (from scrap)         CONTROL FACTORS         Assume Capture to BH           TPH production normalized to prod limit         5937.6 hr/yr         Assume Capture to BH           hV-VOC/ton aluminum (2014 RTI, max delag) <sup>1</sup> 1.14 TPY VHAP         Fug + Build= fugitive after bu           grains DF/ton aluminum (RRR limit)         5.57 F-07 TPY D/F         TPY controller Fugitive           1b NOC/ton aluminum (00% UPL) <sup>6</sup> 1.352 TPY CO         1.46 TPY NOX           1b NOC/ton alu	material handling!*         Fugitives (storage)*           tpy dross & salt cake (Hiake Assumption)         113539 TPY metal scrap           lb pmt/ton low silt         0.021344 TPY pm10         1.3 mph wind           lb pmt/ton low silt         0.021344 TPY pm10         1.3 mph wind           lb pmt/ton low silt         0.00143 TPY pm2.         0.74 pm30factor           0.007554 lb/ton         0.4288 tpy PM         0.0032*PM30*((mph/5)*1.3)/((moist/2)*1.4)           hot dross handling)*         Fugitives (Pouring/Cooling)'         typ dross & salt cake         37,110 Tons Scrap Charged           lb pm10/ton         0.4851 TPY pm10         0.01 lb NO_/ton charged         0.04851 TPY SO2           lb pm10/ton         0.4851 TPY pm2.         0.14 lb VOC/ton charged         0.033957 TPY VOC           ib pm2.5/ton         0.4851 TPY pm2.         0.14 lb VOC/ton charged         0.33957 TPY VOC           ib vhaP/ton aluminum (WebFire)*         3.74 TPY VOC         Assume PCD Efficiency Hake         89.0%           lb VHAP/ton aluminum (WebFire)*         3.74 TPY VPM2.5m         Fug = uncaptured emissions from furma           ratio PM10:PM (filt) (AP42)*         1.59 TPY PM4.5m         PM5.7m         Assume PCD Efficiency Hake         89.0%           hb VOC/ton aluminum (90% UP1)*         5.58 TPY PM4.5m         PM5.7m         Fug = uncaptured emissions from furma	material handling) <sup>4</sup> Fuglitives (storage) <sup>5</sup> tpy dross & salt cake         113539 TPY metal scrap           lb pmt/on low silt         0.01043 TPY pm10           1.3 mph wind         0.025 Kmoisture           lb pm2.5/ton low silt         0.01043 TPY pm20           0.0032*PM30*(Inoist/2)^1.3)/(Inoist/2)^1.3)/(Inoist/2)^1.4)         Image: Im	material handling1         Fugitives (storage) <sup>5</sup> tpy dross & salt cake (Hiake Assumption)         113539 TPY metal scrap           lb pmt/Loftwo low silt         0.02124M TPY pmt0         1.3 mph wind           lb pm2.5/ton low silt         0.003881 TPY pm25         0.07554 lb/ton           0.0032*PM30*((mph/5)*1.3)/((moist/2)*1.4)         0.003881 TPY pm25         0.07554 lb/ton           het dross handling1         Fugitives (construction)         0.023 PPM30*((mph/5)*1.3)/((moist/2)*1.4)           het dross & salt cake         37,110 Tons Scrap Charged         0.0455 TPY NO,           lb pm10/ton         0.4851 TPY pm10         0.01 lb NO,/ton charged         0.04255 TPY NO,           lb pm2.5/ton         0.44851 TPY pm2.5         0.14 lb VOC/ton charged         0.33957 TPY VOC

unused, cited for comparison:

<sup>8</sup>6.0 lb/hr (limit) / 37,110 TPY (charge limit) @ 8760 hrs per year = 1.4 lb-pm/ton charge [Hikae used 1.9 l-pm/ton charge]

	(1) JAW CRUSHER	(1) IMPACT CRUSHER	(1) SCREEN			
Material, Process, Control Type, Particle Size	LOW MOISTURE MINERAL, PRIMARY CRUSHING, UNCONTROLLED	LOW MOISTURE MINERAL, SECONDARY CRUSHING, UNCONTROLLED	STONE, SCREENING, UNCONTROLLED	NO TABULATED FACTOR	NO TABULATED FACTOR	NO TABULATED FACTOR
PMT Emission Factor	0.5	1.2	0.025	NO TABULATED FACTOR	NO TABULATED FACTOR	NO TABULATED FACTOR
PM10 Emission Factor	0.05	0.0087	0.00435	NO TABULATED FACTOR	NO TABULATED FACTOR	NO TABULATED FACTOR
PM2.5 Emission Factor	0.05	0.0087	0.00435	NO TABULATED FACTOR	NO TABULATED FACTOR	NO TABULATED FACTOR
Assumptions	N/A	N/A	PM2.5 = PM10÷2	N/A	N/A	N/A
Number of Emission Points	1	1	1	0	1	0
Capture Efficiency	0.00%	0.00%	0.00%	0.00%	0.00%	0.00%
Control Efficiency	0.00%	0.00%	0.00%	0.00%	0.00%	0.00%
Control Efficiency PM10	0.00%	0.00%	0.00%	0.00%	0.00%	0.00%
Control Efficiency PM2.5	0.00%	0.00%	0.00%	0.00%	0.00%	0.00%
Controlled & captured PT	0	0	0	0	0	0
Controlled & captured PM10	0	0	0	0	0	0
Controlled & captured PM2.5	0	0	0	0	0	0
Fugitive PT	0.500000	1.200000	0.025000	0.000000	0.000000	0.000000
Fugitive PM10	0.050000	0.008700	0.008700	0.000000	0.000000	0.000000
Fugitive PM2.5	0.050000	0.008700	0.004350	0.000000	0.000000	0.000000

BASIS OF EMISSION FACTORS:	AP42 11.24-2	AP42 11.24-2	AP-42 11.19.2	NONE	NONE	NONE
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#### <u>CALCULATIONS (Fugitive Emissions from Crushing and Screening)</u>

hr/yr operation	5937	hours (Normalized to Limit)	Process in Building?	TRUE	
Process Flowrate	7.38	ton/hr	<b>Building Settling Factor</b>	0%	
MHAP fraction of PM	0.50%				
		COMBINED	BINED PM FACTORS TOTAL PM EMISSIONS		EMISSIONS
	РТ	0.00E+00	lb-PM/ton	0.00	ton-PT/yr
K	PM10	0.00E+00	lb-PM/ton	0.00	ton-PM10/yr
ST/	PM2.5	0.00E+00	lb-PM/ton	0.00	ton-PM2.5/yr
	MHAP	0.00E+00	lb-MHAP/ton	0.000	ton-MHAP/yr
Ψ	PT	1.73E+00	lb-PM/ton	37.79	ton-PT/yr
<u>}</u>	PM10	6.74E-02	lb-PM/ton	1.48	ton-PM10/yr
EUG	PM2.5	6.31E-02	lb-PM/ton	1.38	ton-PM2.5/yr
ш	МНАР	8.63E-03	lb-MHAP/ton	0.189	ton-MHAP/yr

	(1) Aluminum Shredder					
Material, Process, Control Type, Particle Size	CUSTOM, CUSTOM, UNCONTROLLED	NO TABULATED FACTOR				
PMT Emission Factor	0.263	NO TABULATED FACTOR				
PM10 Emission Factor	0.116	NO TABULATED FACTOR				
PM2.5 Emission Factor	0.116	NO TABULATED FACTOR				
Assumptions	CUSTOM INPUT	N/A	N/A	N/A	N/A	N/A
Number of Emission Points	1	0	0	0	0	0
Capture Efficiency	0.00%	0.00%	0.00%	0.00%	0.00%	0.00%
Control Efficiency	0.00%	0.00%	0.00%	0.00%	0.00%	0.00%
Control Efficiency PM10	0.00%	0.00%	0.00%	0.00%	0.00%	0.00%
Control Efficiency PM2.5	0.00%	0.00%	0.00%	0.00%	0.00%	0.00%
Controlled & captured PT	0	0	0	0	0	0
Controlled & captured PM10	0	0	0	0	0	0
Controlled & captured PM2.5	0	0	0	0	0	0
Fugitive PT	0.263000	0.000000	0.000000	0.000000	0.000000	0.000000
Fugitive PM10	0.116000	0.000000	0.000000	0.000000	0.000000	0.000000
Fugitive PM2.5	0.116000	0.000000	0.000000	0.000000	0.000000	0.000000

BASIS OF EMISSION FACTORS:	RS NONE	NONE	NONE	NONE	NONE
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#### <u>CALCULATIONS</u>

hr/yr operation	5937	hours (normalized to Limit)	Process in Building?	FALSE	
Process Flowrate	10	ton/hr	<b>Building Settling Factor</b>	0%	
MHAP fraction of PM	0.50%				
		COMBINED	INED PM FACTORS TOTAL PM EMISSION		EMISSIONS
	PT	0.00E+00	lb-PM/ton	0.00	ton-PT/yr
CK	PM10	0.00E+00	lb-PM/ton	0.00	ton-PM10/yr
STA	PM2.5	0.00E+00	lb-PM/ton	0.00	ton-PM2.5/yr
	МНАР	0.00E+00	lb-MHAP/ton	0.000	ton-MHAP/yr
Ē	PT	2.63E-01	lb-PM/ton	7.81	ton-PT/yr
FUGITIVE	PM10	1.16E-01	lb-PM/ton	3.44	ton-PM10/yr
	PM2.5	1.16E-01	lb-PM/ton	3.44	ton-PM2.5/yr
ш	МНАР	1.32E-03	lb-MHAP/ton	0.039	ton-MHAP/yr